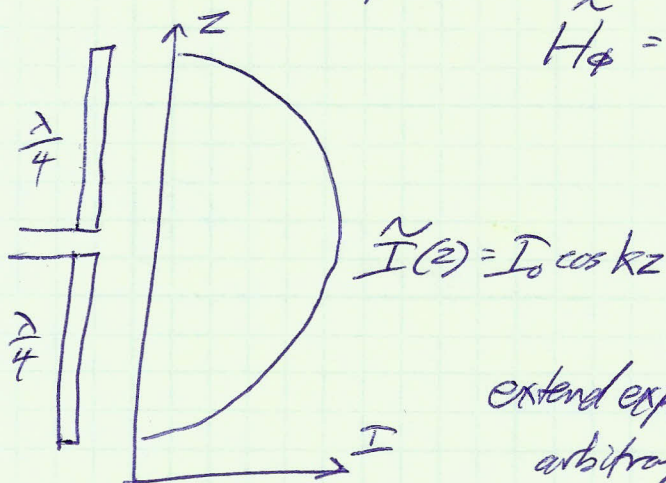


## Half wave dipole antenna

from Hertzian dipole:  $\tilde{E}_\theta = \frac{j I_0 l k \eta_0}{4\pi} \left( \frac{e^{-jkR}}{R} \right) \sin\theta$

$$\tilde{H}_\phi = \frac{\tilde{E}_\theta}{\eta_0}$$

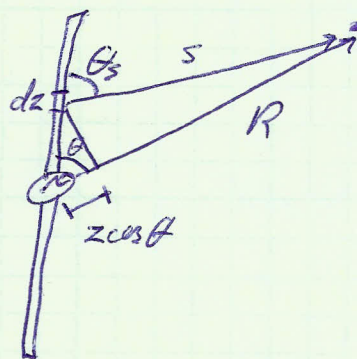


extend expression for  $E, H$  to arbitrary current distribution

$$d\tilde{E}_\theta(z) = \frac{jk\eta_0}{4\pi} \tilde{I}(z) dz \left( \frac{e^{-jks}}{s} \right) \sin\theta$$

$$d\tilde{H}_\phi(z) = \frac{d\tilde{E}_\theta(z)}{\eta_0}$$

$$\tilde{E}_\theta = \int_{-\lambda/4}^{\lambda/4} d\tilde{E}_\theta$$



Two approximations:

①  $\frac{1}{s} \approx \frac{1}{R}$  (very little effect on magnitude)

② for phase term  $s \approx R - z \cos\theta$  (parallel ray approximation)

$$d\tilde{E}_\theta = \frac{jk\eta_0}{4\pi} I(z) dz \left( \frac{e^{-jkR}}{R} \right) \sin\theta e^{jkz \cos\theta}$$

$$\tilde{E}_\theta = \int_{-\lambda/4}^{\lambda/4} \frac{jk\eta_0}{4\pi} \overbrace{I_0 \cos kz}^{\uparrow} \left( \frac{e^{-jkR}}{R} \right) \sin\theta e^{jkz \cos\theta} dz$$

$$= j60 I_0 \left[ \frac{\cos\left[\frac{\pi}{2} \cos\theta\right]}{\sin\theta} \right] \left( \frac{e^{-jkR}}{R} \right) \quad \text{using } \eta_0 \approx 120\pi$$

$$S(R, \theta) = \frac{|\hat{E}_\theta|^2}{2\eta_0} = \underbrace{\frac{15}{\pi} \frac{I_0^2}{R^2}}_{S_0 = S_{\max} = \frac{15}{\pi} \frac{I_0^2}{R^2}} \underbrace{\left[ \frac{\cos^2\left[\frac{\pi}{2} \cos\theta\right]}{\sin^2\theta} \right]}_{F(\theta)}$$

pattern is similar to Hertzian dipole

Directivity of half-wave dipole:

$$P_{\text{rad}} = R^2 \int_{4\pi} S(R, \theta) d\Omega$$

$$= \frac{15 I_0^2}{\pi} \int_0^{2\pi} \int_0^\pi \left[ \frac{\cos^2\left[\frac{\pi}{2} \cos\theta\right]}{\sin^2\theta} \right]^2 \sin\theta d\theta d\phi$$

Must be integrated numerically

$$P_{\text{rad}} \approx 36.6 I_0^2$$

$$D = \frac{4\pi R^2 S_{\max}}{P_{\text{rad}}} = \frac{4\pi R^2}{36.6 I_0^2} \left( \frac{15 I_0^2}{\pi R^2} \right) = 1.64$$

slightly higher than Hertzian dipole, with  $D=1.5$

Radiation resistance:

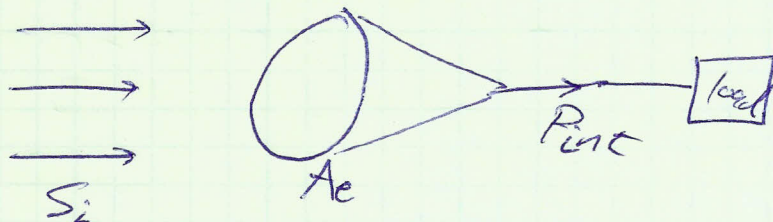
$$R_{\text{rad}} = \frac{2P_{\text{rad}}}{I_0^2} = \frac{2 \times 36.6 I_0^2}{I_0^2} = 73 \Omega$$

This is orders of magnitude greater than Hertzian dipole



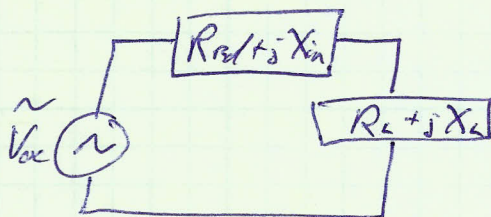
Effective area of receiving antenna

$$A_e = \frac{P_{\text{int}}}{S_i}$$



$$Z_{\text{in}} = R_{\text{rad}} + jX_{\text{in}}$$

$$Z_L = R_L + jX_L$$



for maximum power transfer,  $R_{\text{rad}} = R_L$ ,  $X_{\text{in}} = -X_L$   
equivalent to  $\tilde{V}_{\text{oc}}$  applied to  $2R_{\text{rad}}$

$$P_L = \frac{1}{2} |\tilde{I}_L|^2 R_{\text{rad}} = \frac{1}{2} \left[ \frac{|\tilde{V}_{\text{oc}}|}{2R_{\text{rad}}} \right]^2 R_{\text{rad}} = \frac{|\tilde{V}_{\text{oc}}|^2}{8R_{\text{rad}}}$$

Incident power density:  $S_i = \frac{|\tilde{E}_i|^2}{2\eta_0} = \frac{|\tilde{E}_i|^2}{240\pi}$

$$A_e = \frac{P_{\text{int}}}{S_i} = \frac{30\alpha |\tilde{V}_{\text{oc}}|^2}{R_{\text{rad}} |\tilde{E}_i|^2}$$

For the Hertzian dipole,  $\tilde{V}_{\text{oc}} = \tilde{E}_i l$ , and  $R_{\text{rad}} = 80\pi^2 \left(\frac{l}{\lambda}\right)^2$

$$A_e = \frac{3\lambda^2}{8\pi}$$

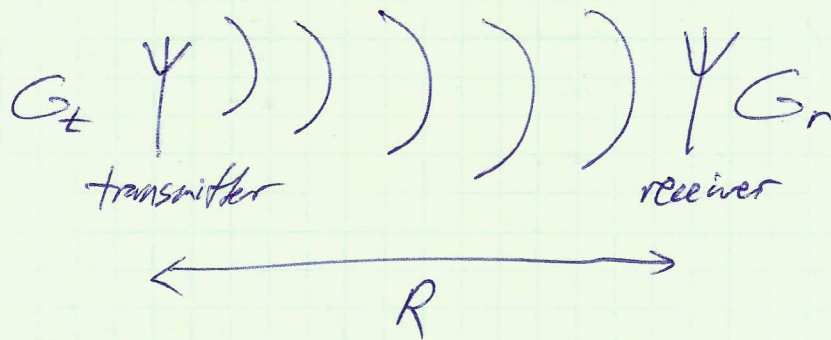
remember that  $D = \frac{3}{2}$  for Hertzian dipole

In general  $A_e = \frac{\lambda^2 D}{4\pi}$

For isotropic antenna,  $A_e = \frac{\lambda^2}{4\pi}$



## Friis Transmission Formula



$$S_{iso} = \frac{P_t}{4\pi R^2}$$

$$S_r = G_t S_{iso} = \frac{G_t P_t}{4\pi R^2} \quad (G_t = \epsilon_t D_t)$$

$$\begin{aligned} P_r &= S_r \cdot A_r \cdot \epsilon_r \\ &= \frac{G_t P_t}{4\pi R^2} \cdot \frac{\lambda^2 D_r}{4\pi} \cdot \epsilon_r \end{aligned}$$

$$\frac{P_r}{P_t} = G_t G_r \left( \frac{\lambda}{4\pi R} \right)^2$$

Example: 100 kW radio station 10 km away, broadcast at 100 MHz

assume  $G_t \approx G_r \approx 1$

$\lambda = 3\text{ m}$  at 100 MHz

$$\left( \frac{3}{4\pi \times 10000} \right)^2 = 5.7 \times 10^{-10}, \text{ or } 92\text{ dB attenuation}$$

$$P_r = 0.000057 \text{ watts}$$